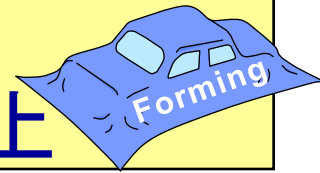
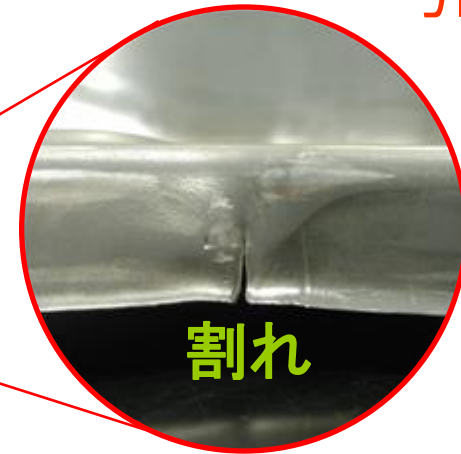
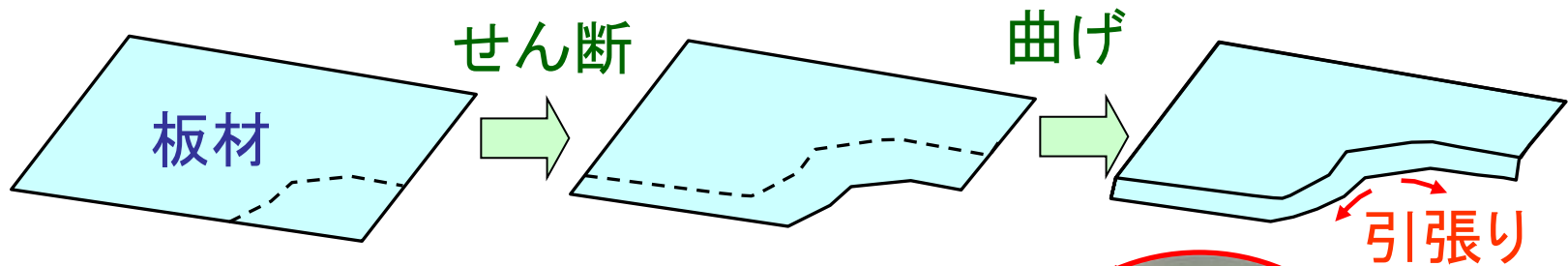


# 17 凹型パンチを用いた2段プレス成形による 超高張力鋼板の伸びフランジ成形性の向上



塑性加工研究室 村田 祐治

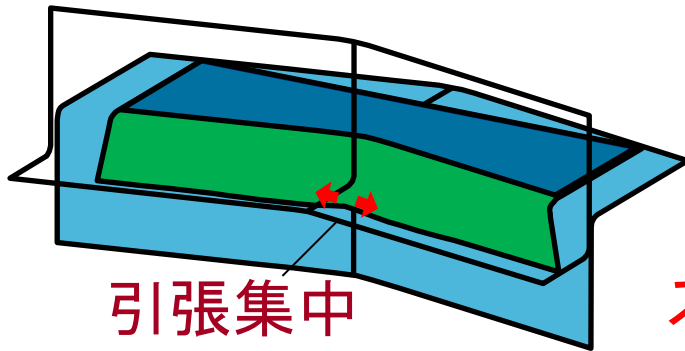
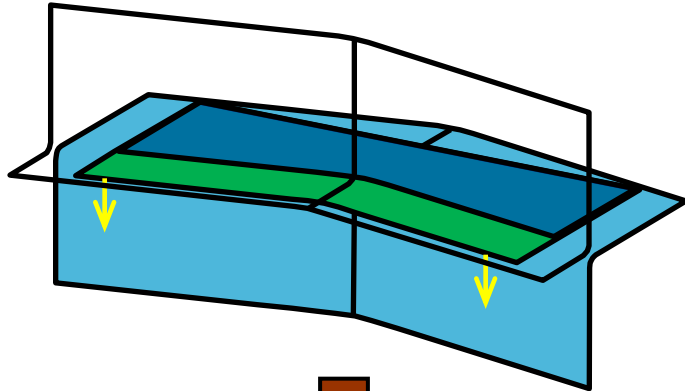
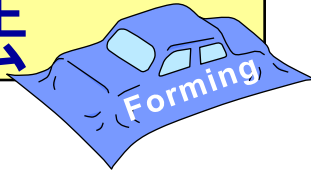


780MPa級高張力鋼板の  
プレス成形部品

超高張力鋼板  
高強度, 低延性

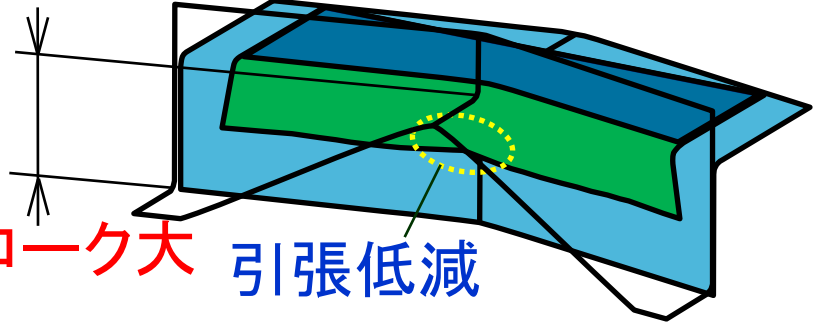
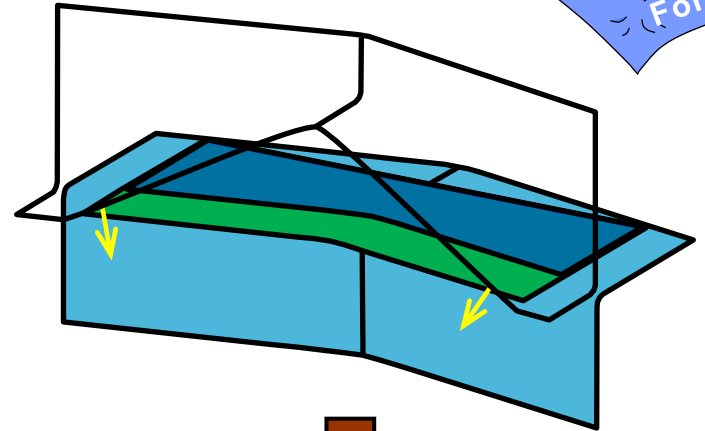
フランジ割れ  
板材端部で発生する  
引張応力による割れ

# 平坦および逐次接触パンチによる成形法



引張集中

(a) 平坦パンチ



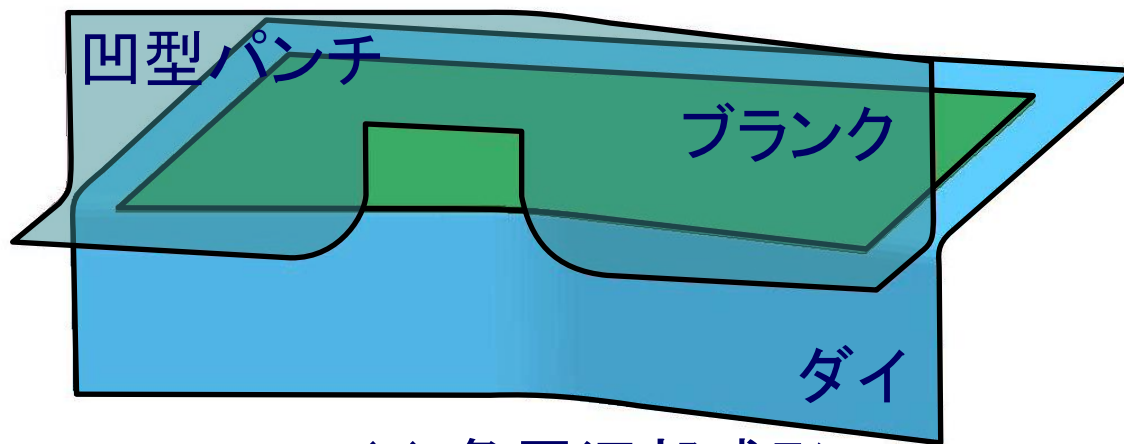
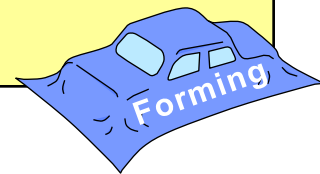
ストローク大 引張低減

(b) 逐次接触パンチ

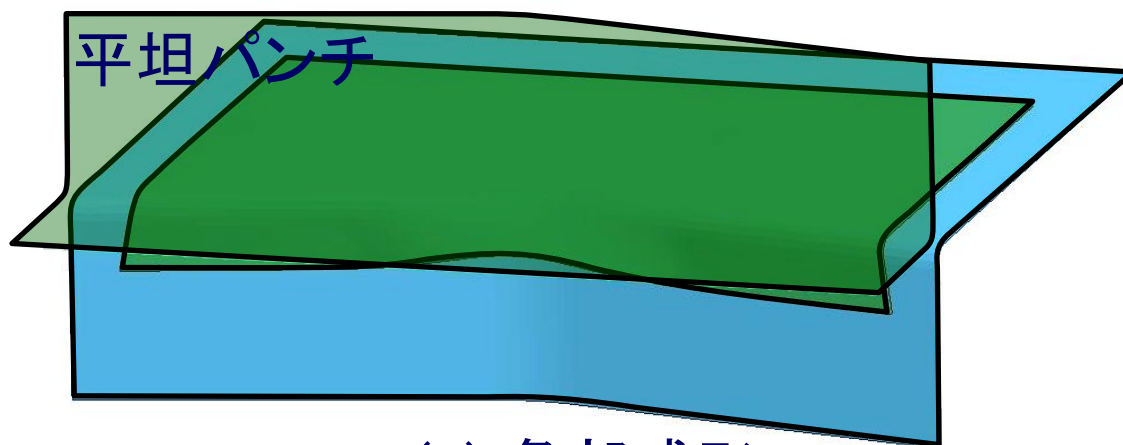
## 目的

凹型パンチを用いた2段伸びフランジ成形法による伸びフランジ角部の伸びの抑制、および割れの防止

# 2段伸びフランジ成形法

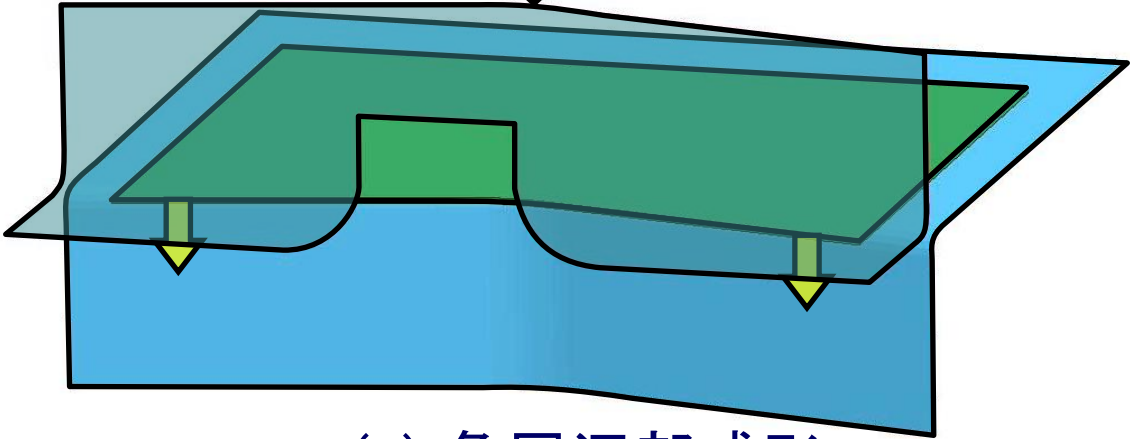
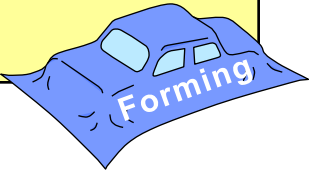


(a) 角周辺部成形

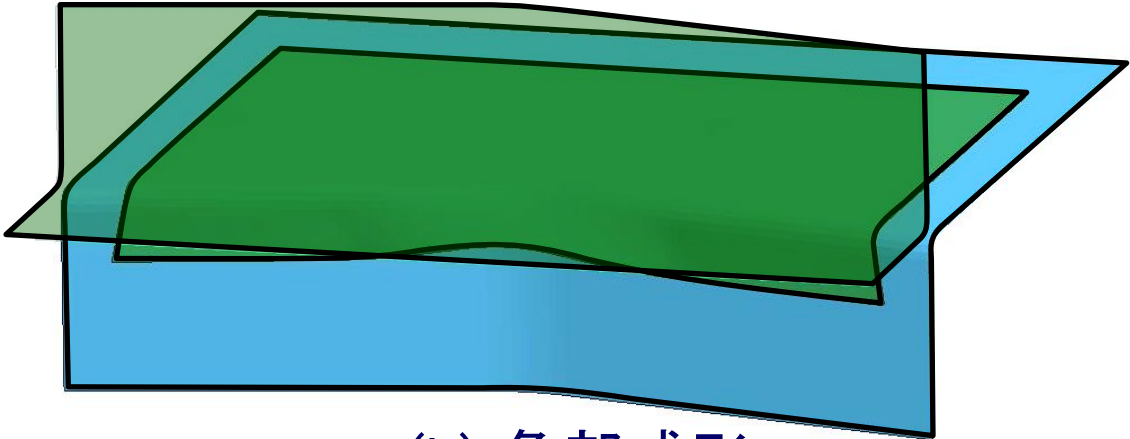


(b) 角部成形

# 2段伸びフランジ成形法

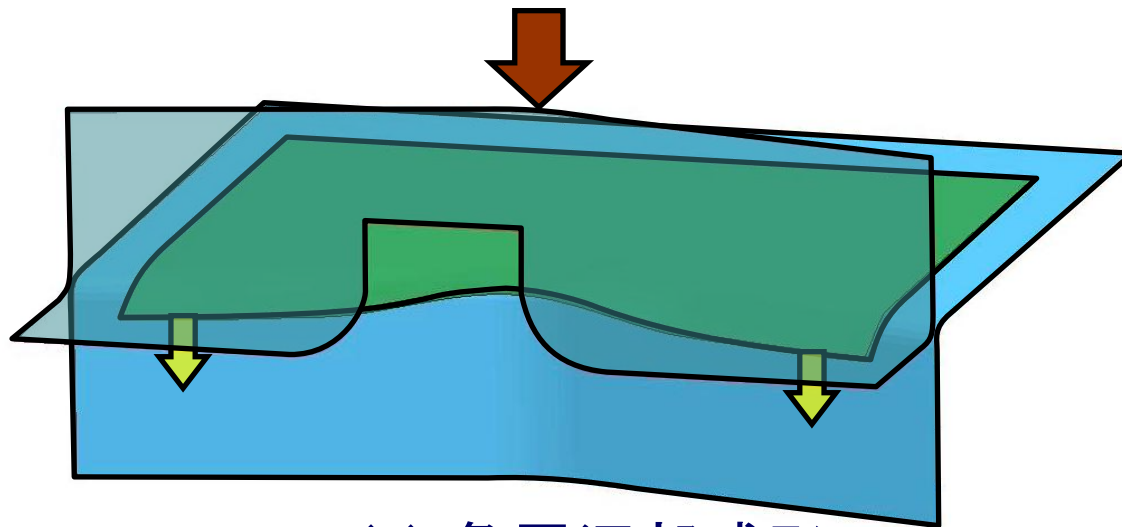
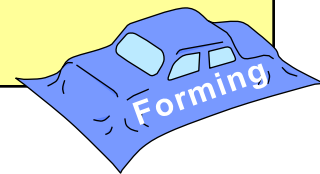


(a) 角周辺部成形

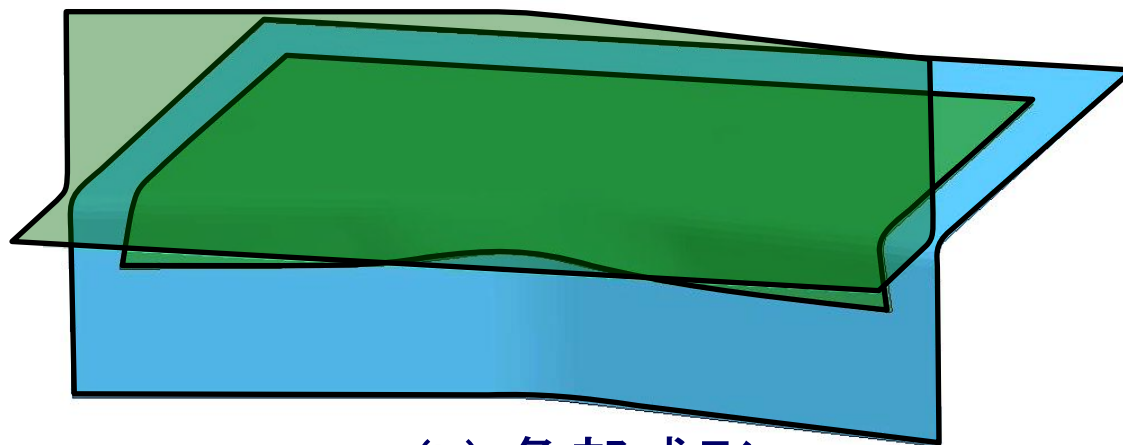


(b) 角部成形

# 2段伸びフランジ成形法

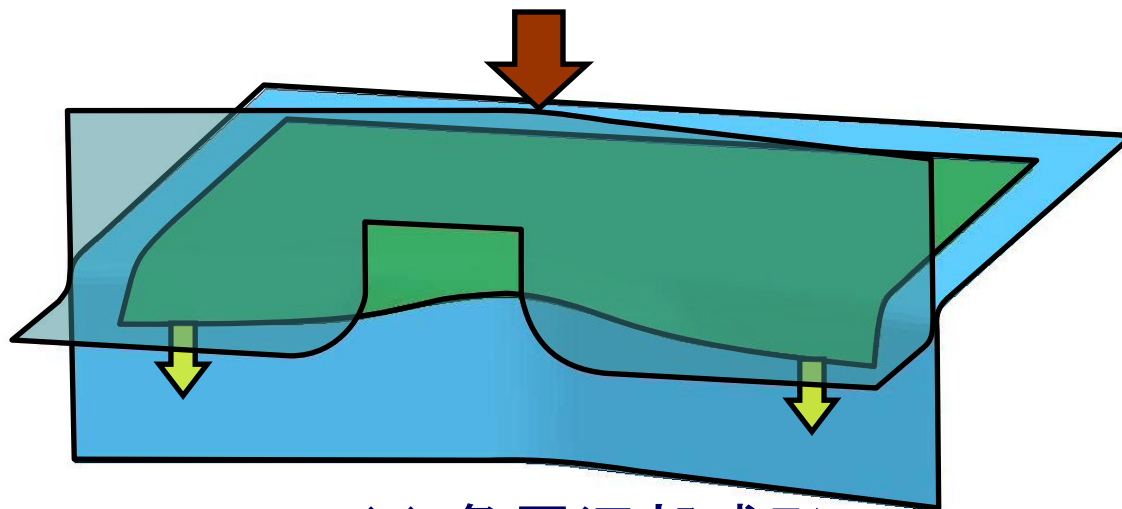
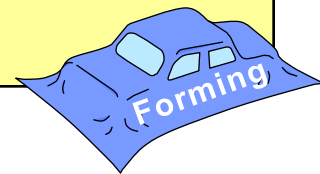


(a) 角周辺部成形

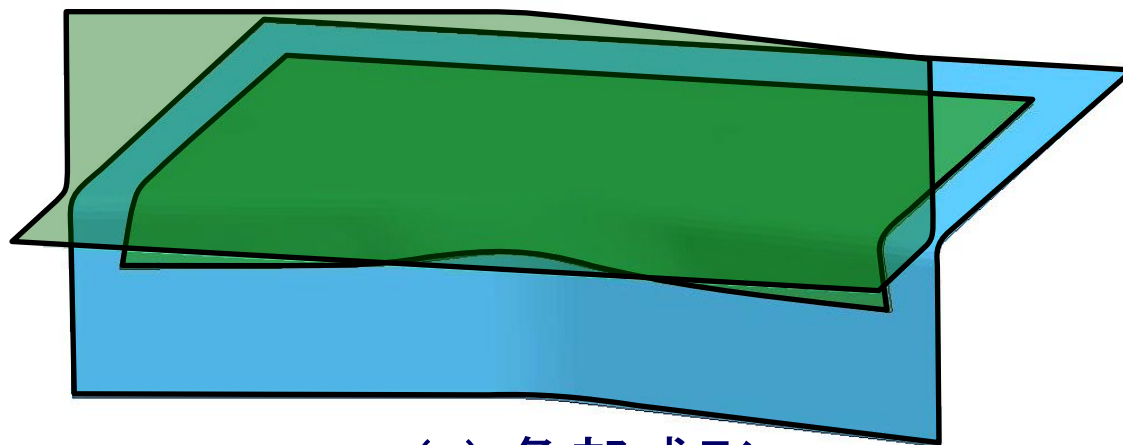


(b) 角部成形

# 2段伸びフランジ成形法

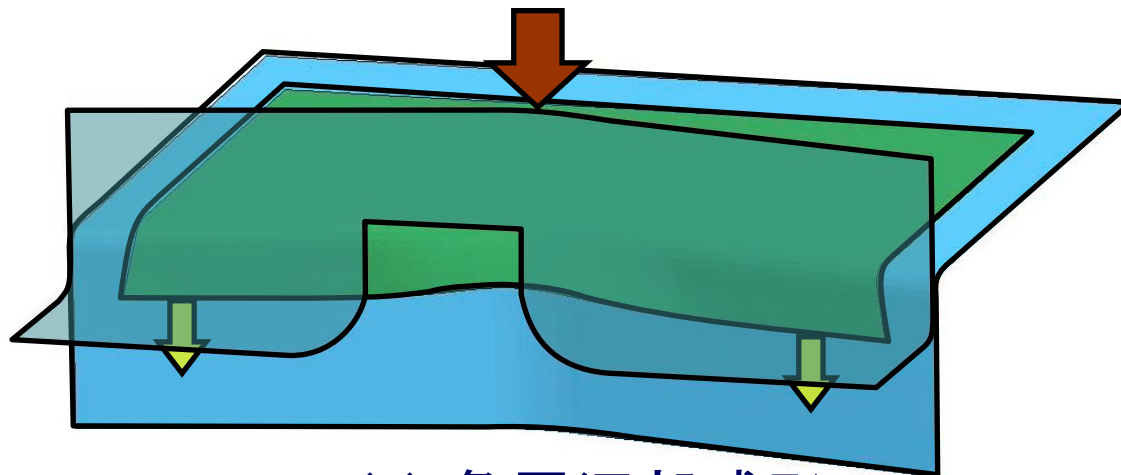
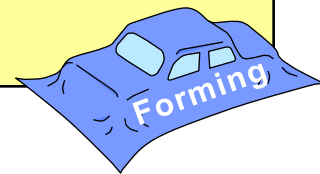


(a) 角周辺部成形

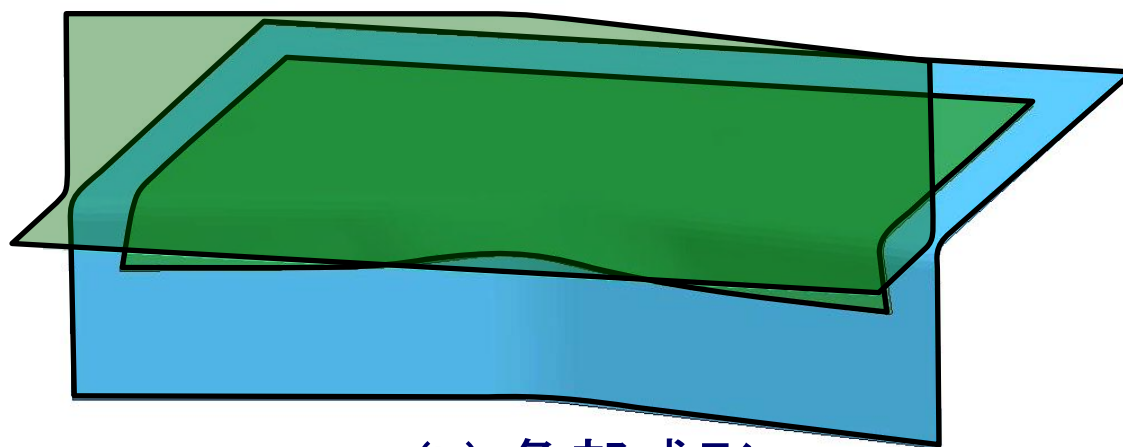


(b) 角部成形

# 2段伸びフランジ成形法

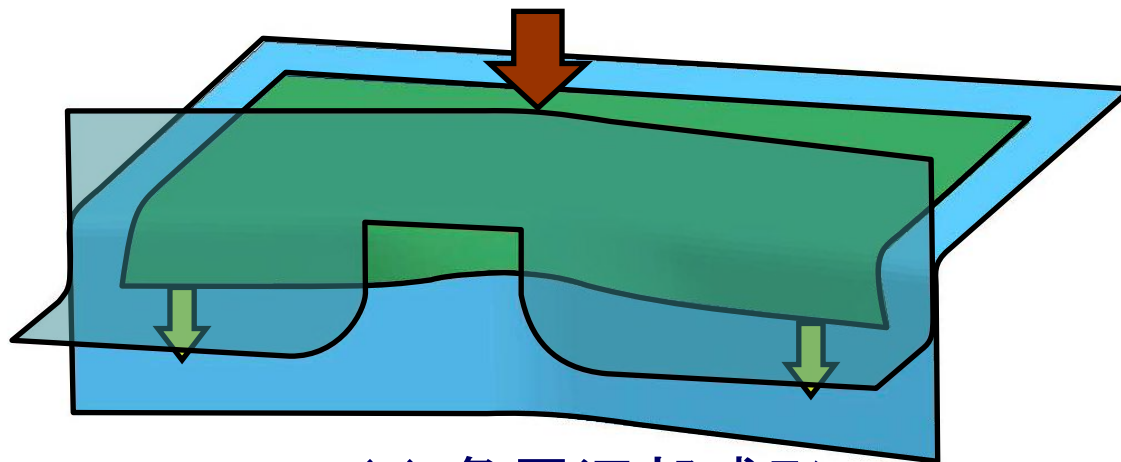
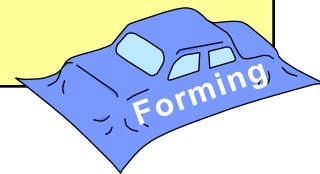


(a) 角周辺部成形

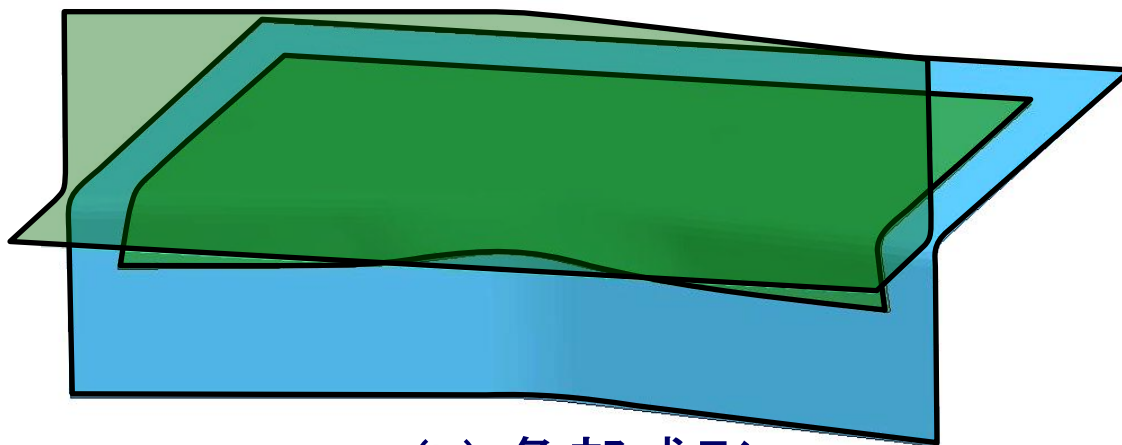


(b) 角部成形

# 2段伸びフランジ成形法



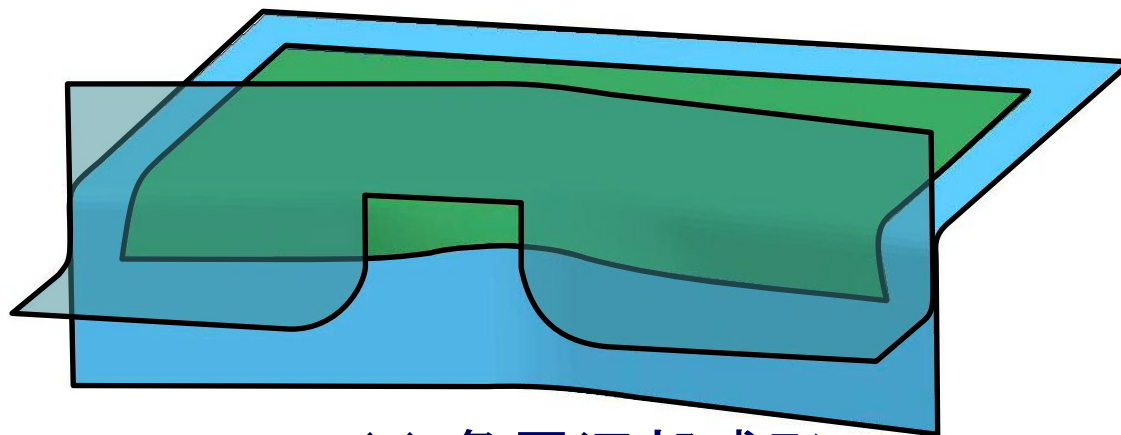
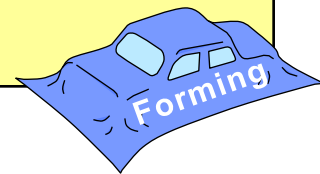
(a) 角周辺部成形



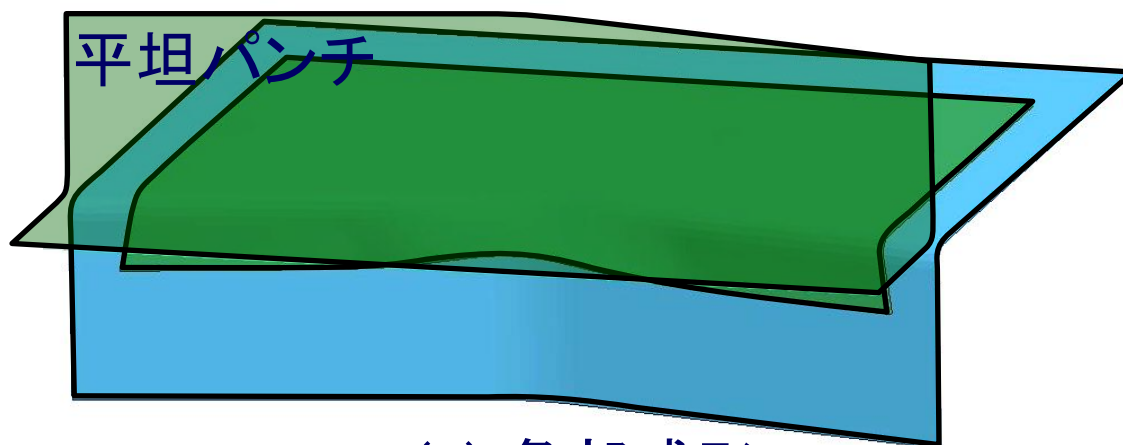
(b) 角部成形



# 2段伸びフランジ成形法

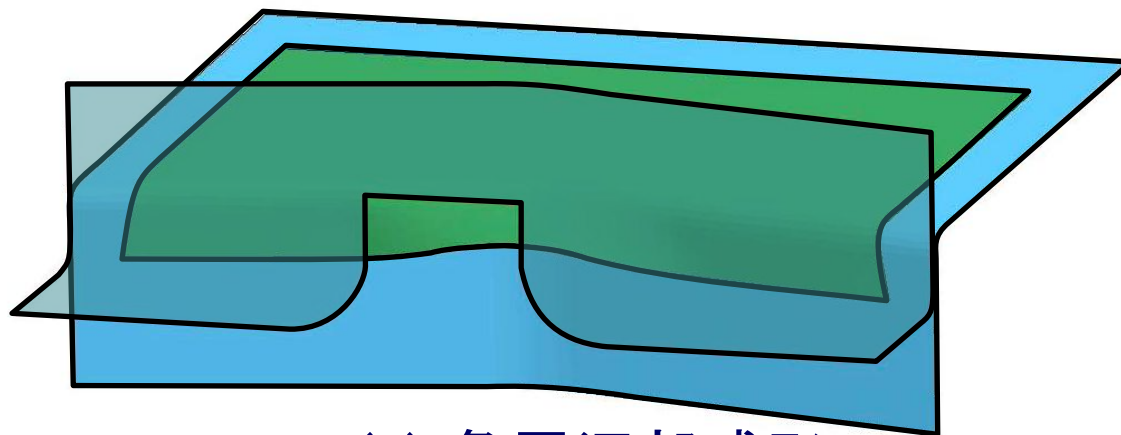
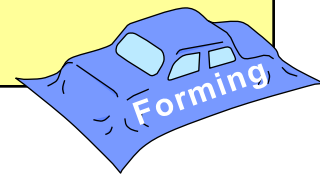


(a) 角周辺部成形

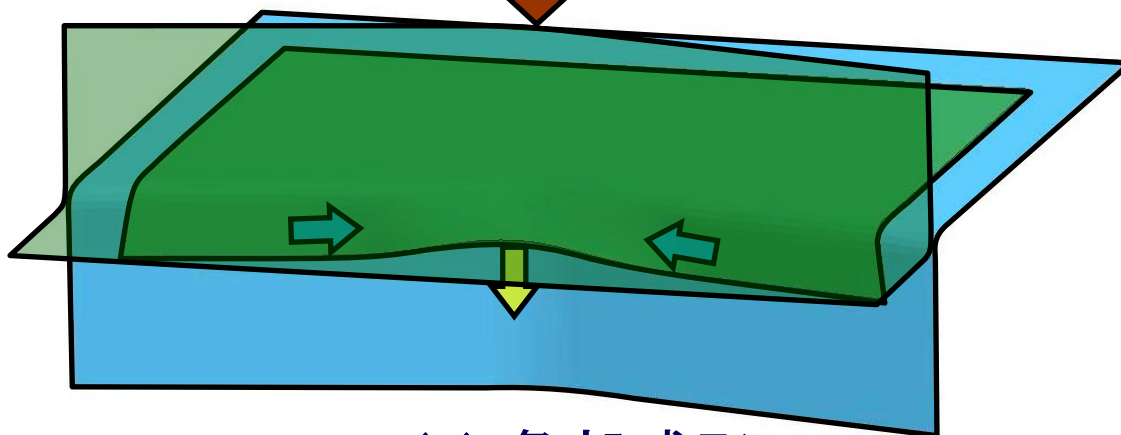


(b) 角部成形

# 2段伸びフランジ成形法

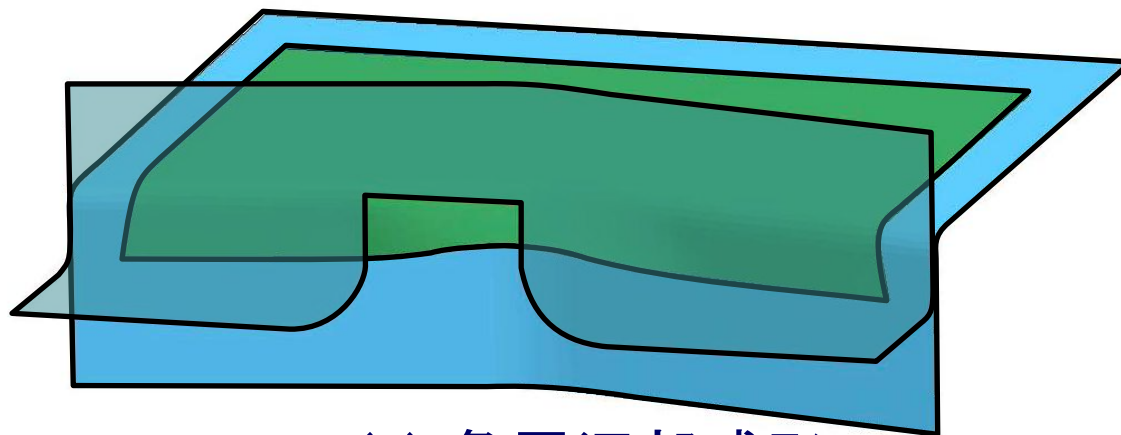
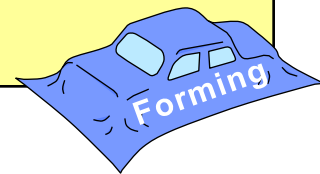


(a) 角周辺部成形

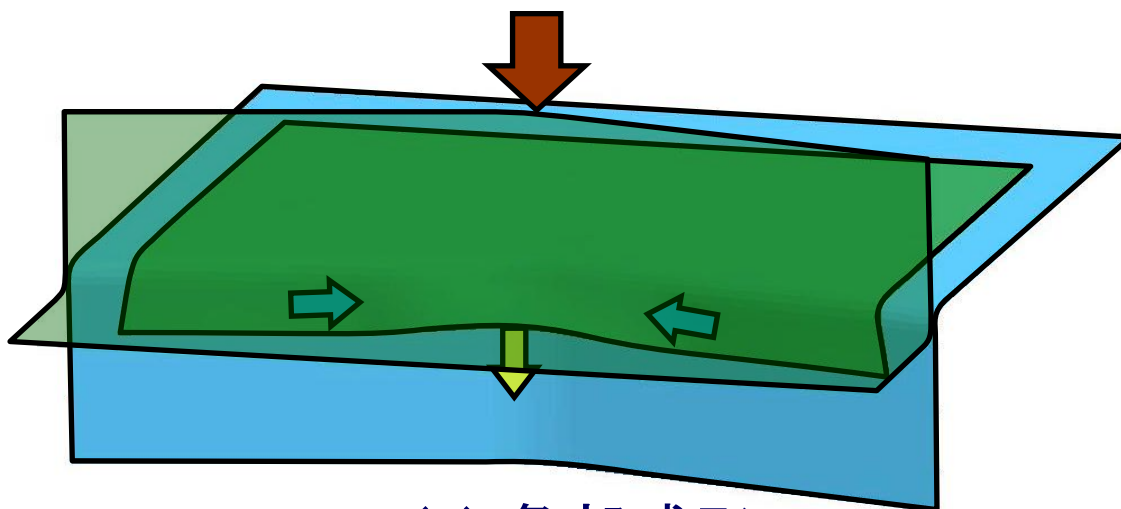


(b) 角部成形

# 2段伸びフランジ成形法

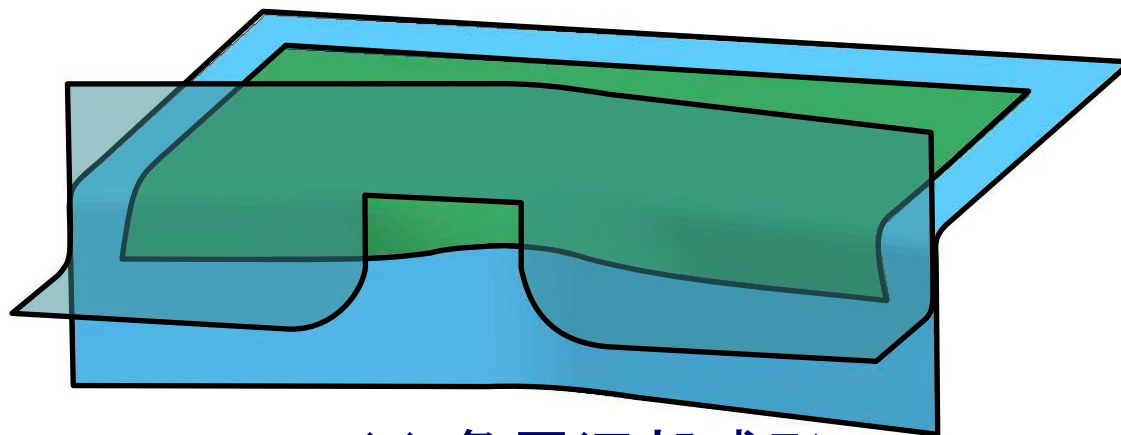
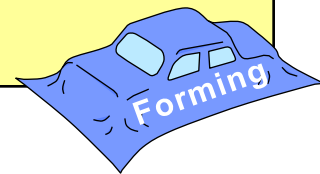


(a) 角周辺部成形

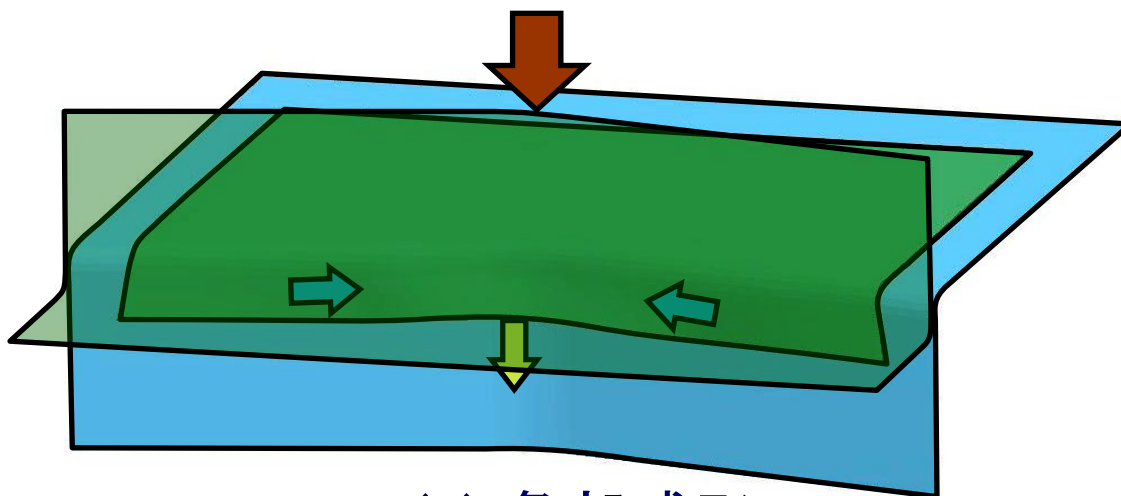


(b) 角部成形

# 2段伸びフランジ成形法

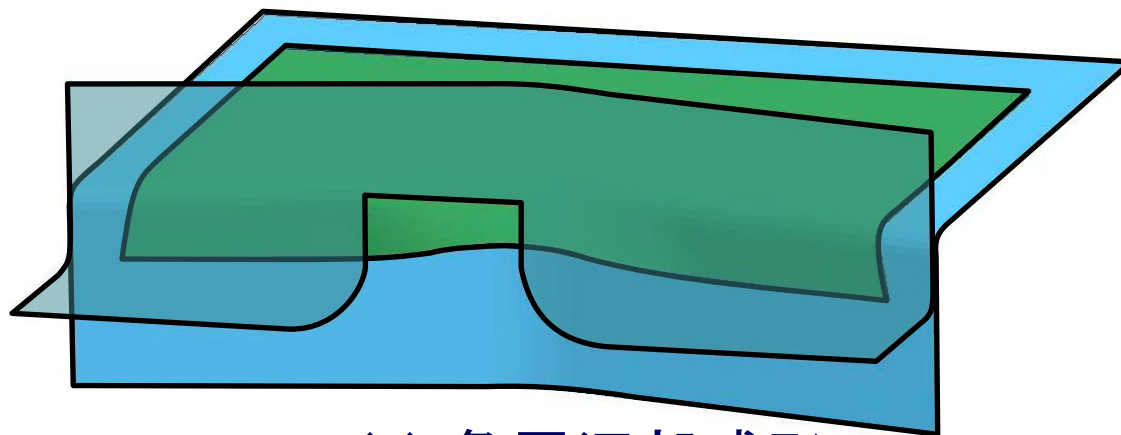
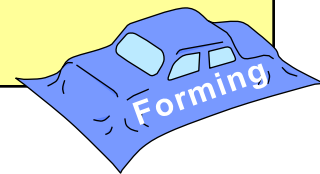


(a) 角周辺部成形

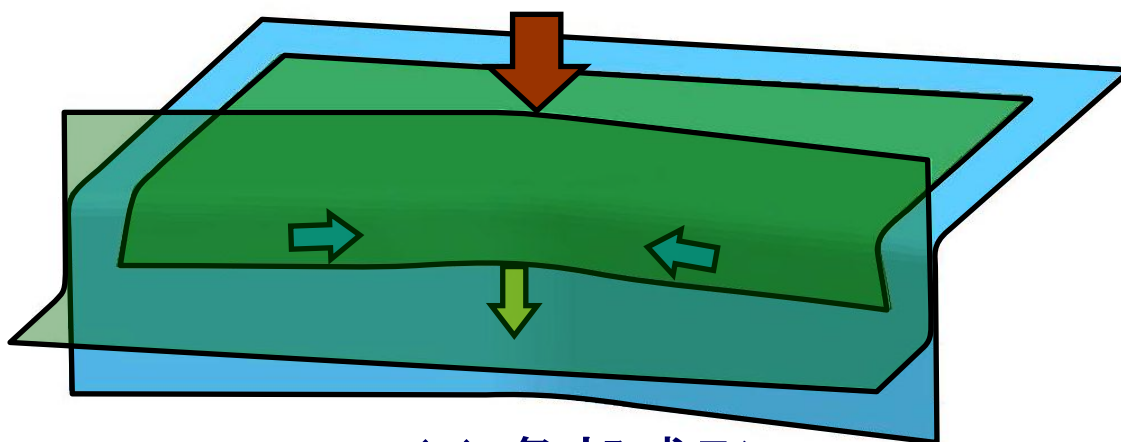


(b) 角部成形

# 2段伸びフランジ成形法

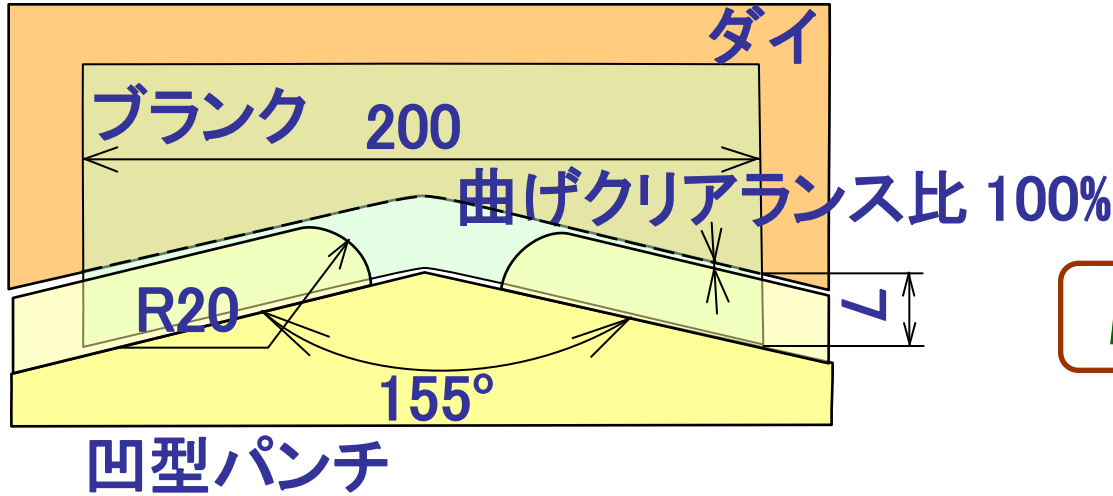
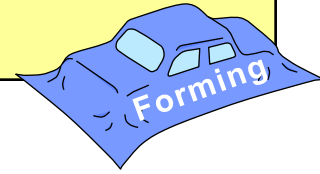


(a) 角周辺部成形

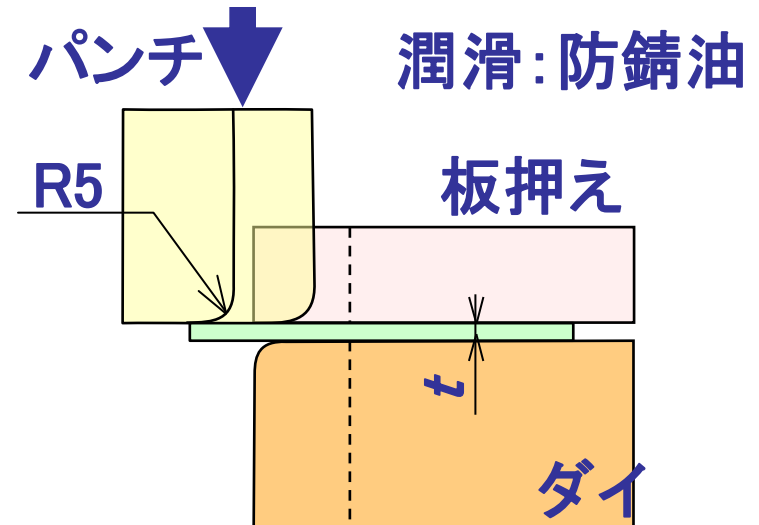
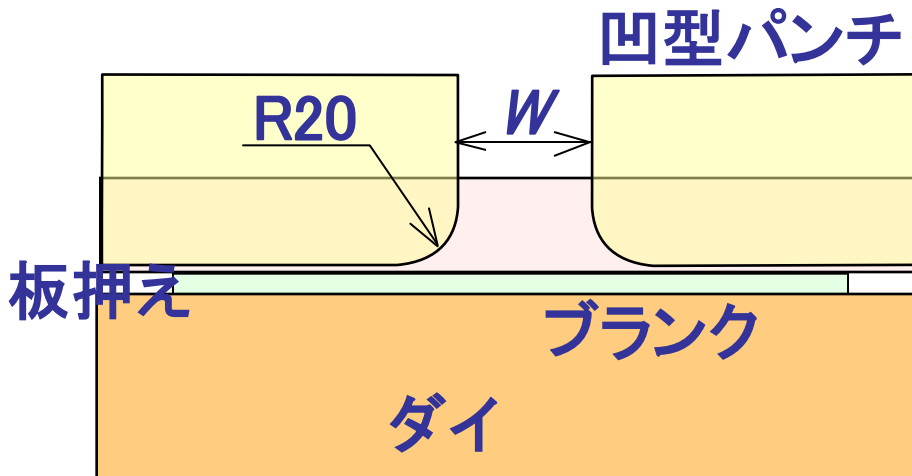


(b) 角部成形

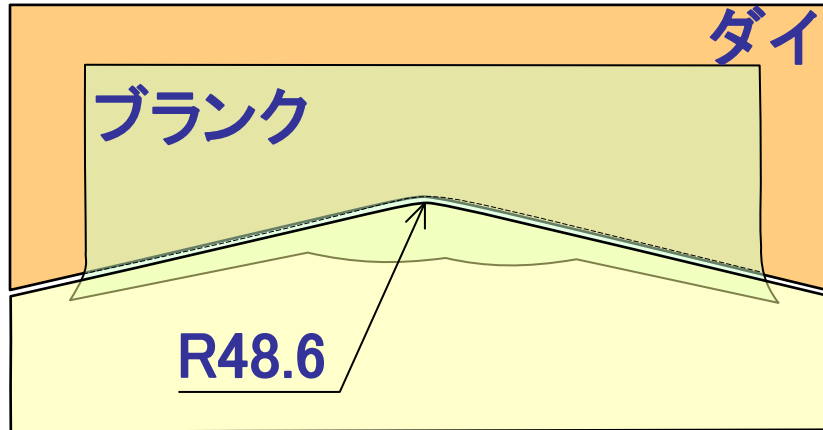
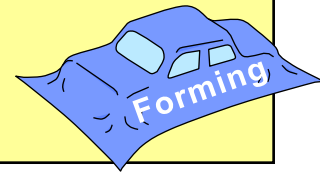
# 角周辺部成形条件



$W=10, 30, 40, 50\text{mm}$



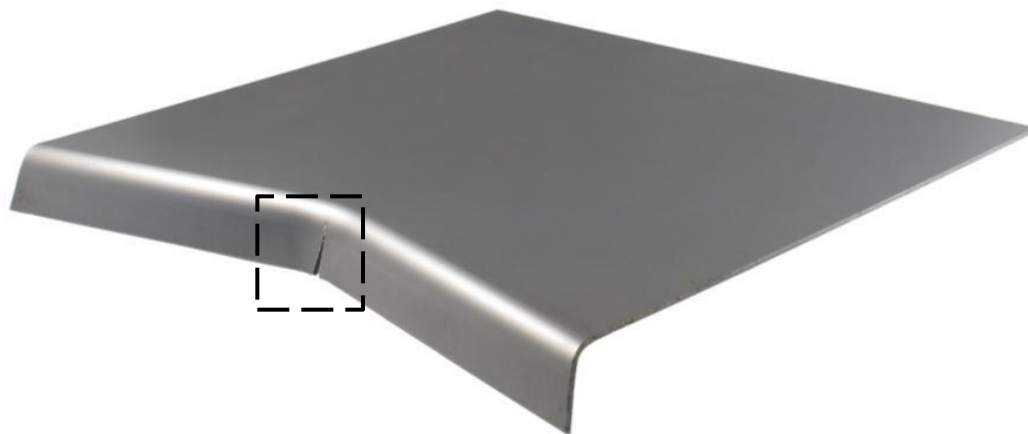
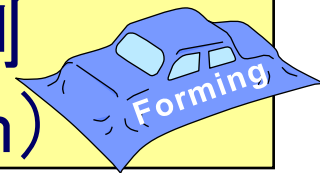
# 角部成形条件および 超高張力鋼鈹の機械的性質



平坦パンチ

	板厚 /mm	引張強さ /MPa	伸び /%
JSC980	1.22	1051	13
	1.43	1014	16.4
JSC1180	1.22	1250	8

# 2段伸びフランジ成形による割れの抑制 (JSC1180, $t=1.22\text{mm}$ , $L=15.5\text{mm}$ , $W=10\text{mm}$ )



成形後のブランク

割れあり



(a) 平坦

割れ無し

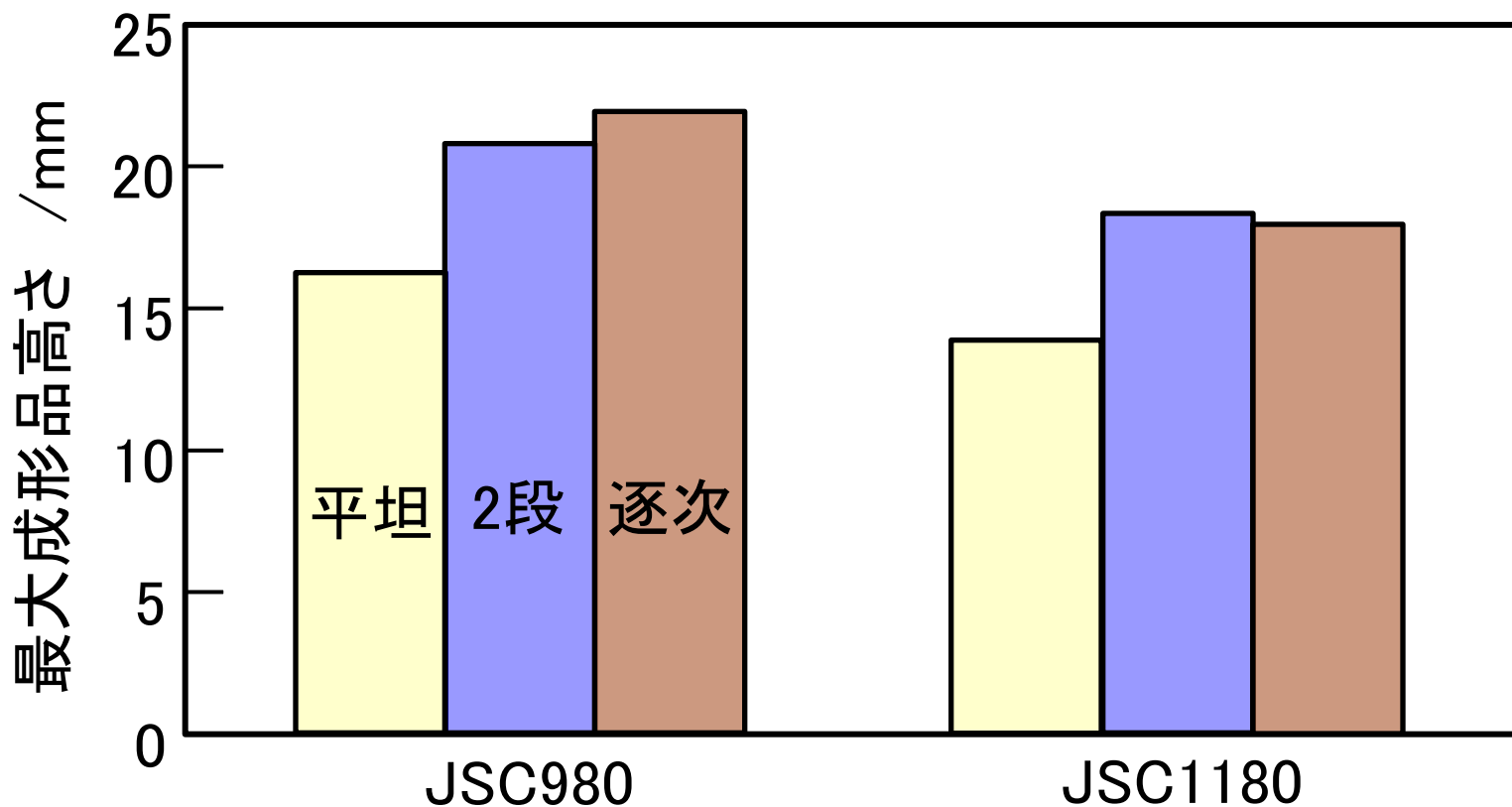
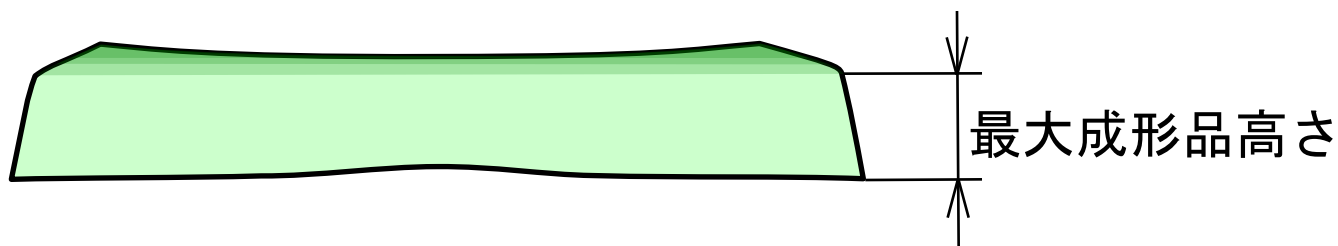
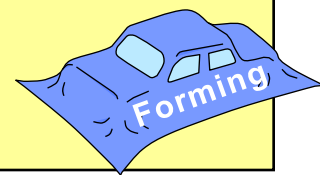


(b) 2段成形

2mm  
H

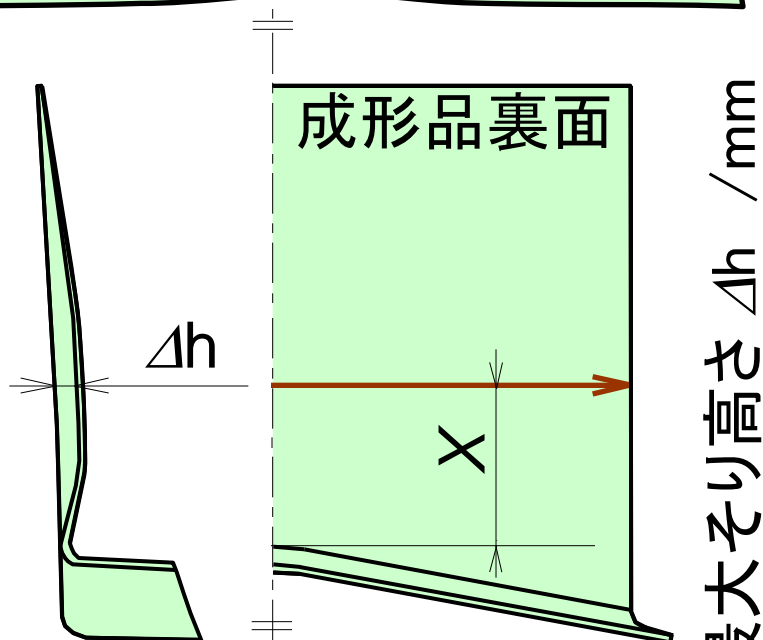
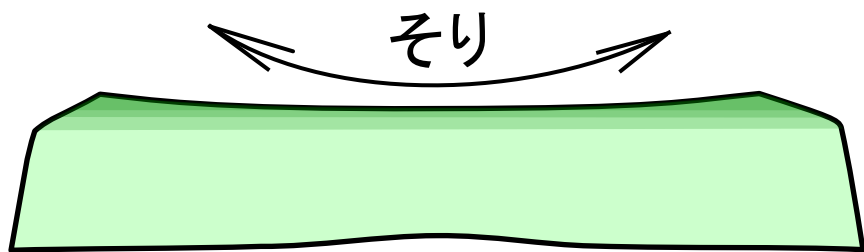
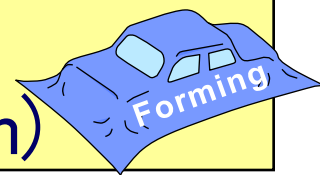


# 実験における最大成形品高さの向上 ( $t=1.22\text{mm}$ , $W=10\text{mm}$ )

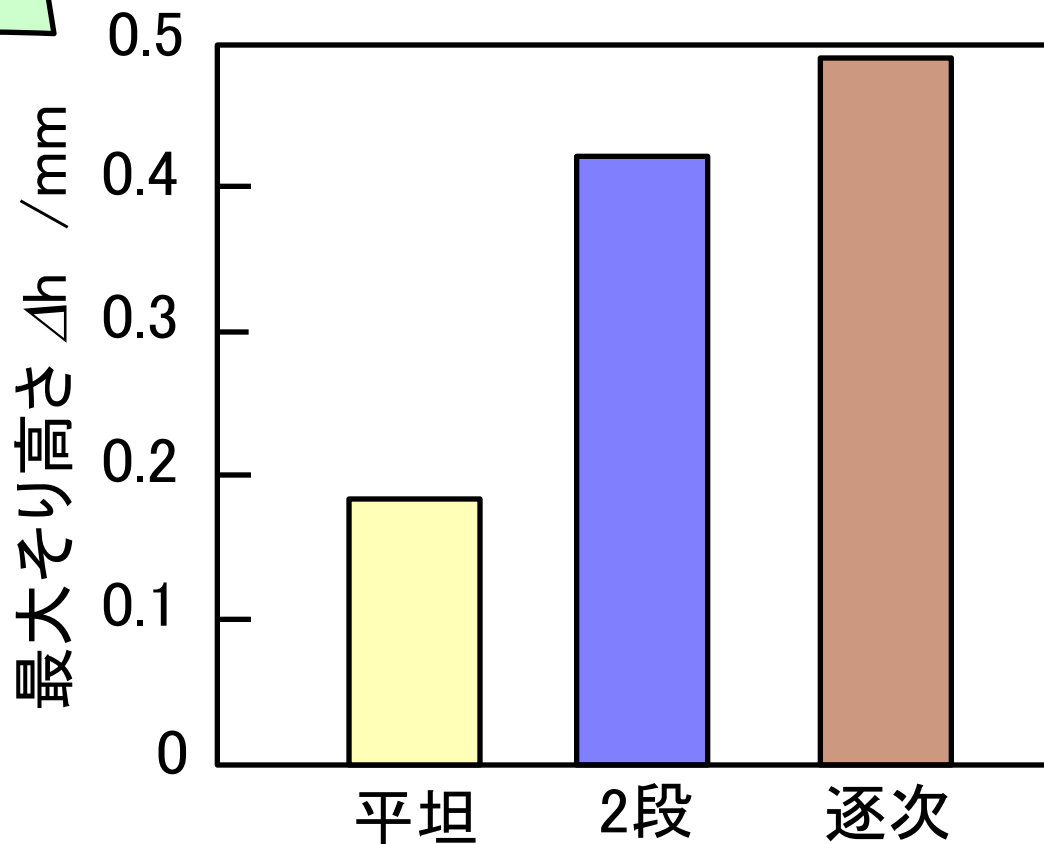


# 実験における成形品のそり

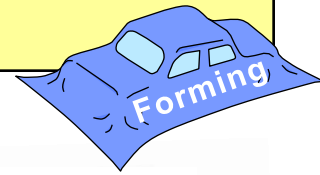
(JSC980,  $t=1.43\text{mm}$ ,  $L=13.5\text{mm}$ ,  $W=40\text{mm}$ )



測定箇所



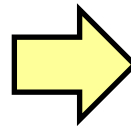
# 塩酸浸漬実験による遅れ破壊の調査



9時間, 塩酸浸漬

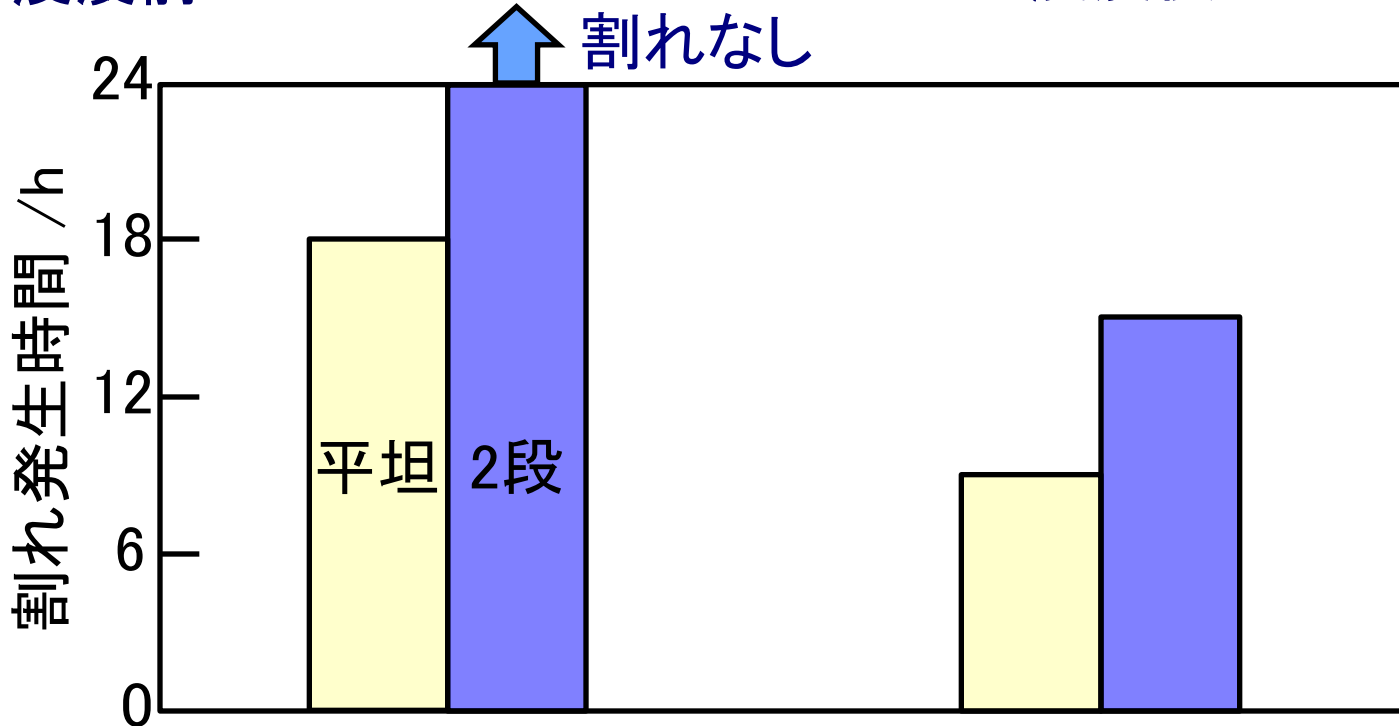


浸漬前



浸漬後

割れなし

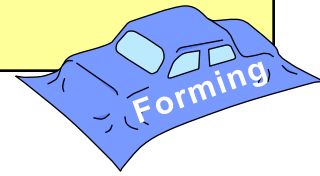


割れ

JSC980,  $t = 1.43\text{mm}$ ,  
 $L = 13.5\text{mm}$ ,  $W = 40\text{mm}$

JSC1180,  $t = 1.22\text{mm}$ ,  
 $L = 12.5\text{mm}$ ,  $W = 10\text{mm}$

# 結 言



- 凹型パンチを用いて2段伸びフランジ成形を行うことで、980MPa級と1180MPa級の超高張力鋼板において、最大成形品高さがそれぞれ28%と32%向上できた。
- 2段伸びフランジ成形では、逐次接触パンチによる成形に比べそりを低減できた。
- 2段伸びフランジ成形を行うことにより、遅れ破壊による割れの発生を抑制できた。